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Abstract— Over recent years, regression model is a well known modeling technique used to model the real world application. This paper conducted computational experimental study using two types of regression models; second order polynomial regression (SOP) and multiple linear regression in optimizing machining process parameters of cobalt-bonded tungsten carbide (WC/Co) electrical discharge machining (EDM). Multiobjective genetic algorithm (MOGA) is widely known in optimization researches. Therefore, combination of conventional modeling (regression) and modern optimization (MOGA) techniques, MLR-MOGA and SOP-MOGA are examined to observe the capability of these two techniques in maximizing removal rate (MRR) and minimizing surface roughness (Ra). Four parameters are considered to create correlation with the machining performances. The best removal rate and surface roughness values are obtained from MLR-MOGA; 168.212 mg/min and 0.693 µm respectively. Nevertheless, SOP-MOGA produced viable results. The results of MLR-MOGA and SOP-MOGA benefits the machine operators or engineers when various combination of machining parameters can be selected based on the desired requirements.

Keywords — Machining, Genetic Algorithm, Regression, Multiobjective

## I. INTRODUCTION

Machining can be divided into two categories; (i) modern machining and (ii) traditional machining. Known as the earliest modern machining, EDM is a well established machining option used to remove material through the action of electrical discharge in fast mode and high current density. One of EDM research interests is optimizing the process parameters as highlighted by Ho and Newman [1].

Machining models are developed to represent the connection between input (machining parameters) and output (machining performances) variables. There are many

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modeling techniques in machining optimization such as fuzzy logic [2], support vector machine [3], artificial neural network (ANN) [4] and many more.

New soft computing techniques are developed to assist in searching optimal solutions such as genetic algorithm (GA) [5], Levi flight algorithm [6], glowworm swarm optimization [7], firefly algorithm [8] and many more. GA is one of the most popular techniques in the machining optimization area as studied by Yusup et al. [9]. Multi objective GA is an optimization technique that is enhanced from single objective genetic algorithm to support the multi objectives problems. One of the pioneer in multi objective GA; MOGA [10] implemented a rank based fitness assignment and nicheformation methods to encourage the search toward Pareto front in the optimization algorithm. According to the theory of Fonseca and Fleming [10], all non dominated individuals are assign rank 1 as in Figure 1.



Fig. 1. Multiobjective ranking

In 2002, Deb et al. introduced a modified version of multiobjective GA, NSGA-II [11] which is highly applied in machining optimization [12]. Bouzakis et al [13] minimized milling machining cost and machining time with consideration

of three parameters, (i) depth of cut, (ii) feed rate and (iii) cutting speed. The authors used MOGA technique to obtain the process parameters that can be applied in various cases of milling optimization process. Mahdavinejad [14] optimized the turning parameters of steel using MOGA and multiobjective harmony search (HS) algorithm Geem et al. [15] to optimize removal rate and surface roughness. Sultana and Dhar [16] used response surface methodology (RSM) to develop machining model and MOGA to optimize the process parameters of turning AISI-4320 steel by uncoated carbide insert. The process parameters considered are cutting speed, feed rate, pressure and flow rate of high pressure and the objectives considered are cutting temperature, chip reduction co-efficient and surface roughness. Venkataraman [17] maximized removal rate and minimized electrode wear rate (EWR) for EDM. Five parameters considered are open voltage, pulse on time, duty cycle and pressure of flushing fluid. Polynomial model and multi objective genetic algorithm are used to optimize the machining process.

Kanagarajan et al. [18] employed second order polynomial regression and non dominated sorting genetic algorithm (NSGA-II) to optimize the machining parameters of WC/Co EDM. Yusoff et al. [19] then applied the model developed by Kanagarajan et al. using both; single (SoGA) and multi objective optimization techniques (MOGA and NSGA-II). It is found that SoGA produced the lowest surface roughness value and the results obtained from MOGA are viable compared to NSGA-II. In conjunction with the experimental conducted by Yusoff et al. [19], this study investigated and compared the efficiencies of regression modeling techniques in optimizing of WC/Co EDM parameters using MOGA. Basically, this study is conducted to observe the performances of two different regression models when integrated with MOGA in machining optimization.

#### II. RESEARCH METHODOLOGY

Essentially, this study employed four consecutive ways in obtaining the final optimal solutions. The steps involved; collection of experimental data, modeling, optimization and results analysis. Second order polynomial (SOP) and multiple linear regression (MLR) are used to obtain the machining models. Multiobjective GA (MOGA) is used to optimize the parameters. Using computational and soft computing techniques in obtaining optimal solutions can reduce the machining trials that involved extreme cost, time and attempt in searching the best parameters.

The parameters considered are electrode rotation (R), current (I), pulse on time (T) and dielectric flushing pressure (P). Removal rate (MRR) and surface roughness (Ra) are the machining objectives or also known as the machining performances.

To correlate the machining inputs (machining parameters) and outputs (machining performances), two types of regression models are applied. Second order polynomial regression (SOP) developed by Kanagarajan et al. and multiple linear regression (MLR) which is developed using SPSS software. The models are then integrated in the optimization tool, MOGA using Matlab software to obtain the optimal solutions.

Finally the results of these two techniques are compared. The flow of this study is summarized as shown in Figure 2 and further details in next sub-sub sections.



Fig. 2. Research flow

#### A. Experimental

The experimental results by Kanagarajan et al. [18] are used in this study. The authors used a machine of Electronica die sinking EDM (M100 model, Electronica, India) with a transistor switched power supply. Density for WC is 15.7 g/cc and CO is 13.55 g/cc. The grain sizes are  $6\mu m$  and  $3\mu m$  respectively. The machining conditions of this study are shown in Table I.

TABLE I. MACHINING CONDITIONS

Condition	Descriptions
Electrode	Material: copper (electrolytic grade)
	Size: cylindrical with a diameter of 13 mm
Workpiece	Material: tungsten carbide 70% WC/ 30% Co
	Size: cylindrical rod of diameter 13 mm
	Dielectric fluid: kerosene
Flushing	Jet flushing
	Flushing pressure: 0.5-1.5
Rotational speed	250, 500, 1000 rpm
Discharge current	5, 10, 15 A
Pulse on time	200, 500, 1000

The experimental results of WC/Co EDM as shown in Table II are based on L27 orthogonal array technique covering full range of current setting with pulse on time settings.

Sol.	Electrode	Current,	Pulse on	Flushing	MRR,	Ra,
	Rotation,	A (I)	time, µs	pressure,	mg/min	μm
	rpm (R)		(T)	$kg/cm^{2}(P)$	_	-
1	250	5	200	0.5	38.19	3.94
2	250	5	200	1.0	46.05	2.84
3	250	5	200	1.5	51.37	2.35
4	250	10	500	0.5	46.50	8.83
5	250	10	500	1.0	56.07	6.37
6	250	10	500	1.5	62.56	5.27
7	250	15	1000	0.5	49.31	14.74
8	250	15	1000	1.0	59.45	10.64
9	250	15	1000	1.5	66.33	8.80
10	500	5	500	0.5	37.77	3.89
11	500	5	500	1.0	45.54	2.81
12	500	5	500	1.5	50.81	2.39
13	500	10	1000	0.5	49.84	8.24
14	500	10	1000	1.0	60.09	5.94
15	500	10	1000	1.5	67.05	4.91
16	500	15	200	0.5	121.07	7.56
17	500	15	200	1.0	145.98	5.45
18	500	15	200	1.5	162.87	4.51
19	1000	5	1000	0.5	40.48	3.63
20	1000	5	1000	1.0	48.81	2.62
21	1000	5	1000	1.5	54.46	2.37
22	1000	10	200	0.5	122.37	4.22
23	1000	10	200	1.0	147.55	3.05
24	1000	10	200	1.5	164.62	2.52
25	1000	15	500	0.5	119.74	7.47
26	1000	15	500	1.0	144.38	5.39
27	1000	15	500	1.5	161.09	4.46
Max	removal rate	(MRR)			164.62	
Min surface roughness (Ra)						2.35

TABLE II. EXPERIMENTAL RESULTS OF WC/CO EDM

#### B. Machining Models

From the machining results, two models are implemented; (i) second order polynomial model developed by Kanagarajan et al. [18] and (i) newly developed multiple linear regression model (MLR). The second order polynomial models for removal rate and surface roughness are shown in Equation 1 and Equation 2 for material removal rate (MRR) and surface roughness (Ra) respectively.

Second Order Polynomial Regression MRR = -30.3660 + 0.1589R + 9.5259I - 0.1241T + (1)  $20.8585P - 0.0001R^2 - 0.2318I^2 + 0.0001T^2 9.2131P^2 - 0.0002RI - 0.0000RT + 0.0220RP +$ 1.9991IP - 0.0199TP

$$Ra = 4.2307 - 0.0116S + 0.5816C + 0.0099T - (2)$$
  

$$4.7481P + 0.0000S^{2} + 0.0085C^{2} - 0.0000T^{2} +$$
  

$$2.1239P^{2} - 0.0002SC - 0.0000ST - 0.0020SP -$$
  

$$0.2462CP - 0.0018$$

Multiple linear regression equations of removal rate and surface roughness are based on the unstandardized coefficients values (B) of Tables III and IV.

TABLE III. COEFFICIENTS VALUES FOR MRR

Model	Unstandardized	Coefficients
Widdel	В	Std. Error
(Constant)	-15.652	8.295
R	0.075	0.006
Ι	6.853	0.461
Т	0.068	0.006
Р	23.988	4.607

 $TABLE \ IV. \ \ COEFFICIENTS \ VALUES \ FOR \ RA$ 

Madal	Unstandard	lized Coefficients
Model	В	Std. Error
(Constant)	3.734	0.815
R	-0.004	0.001
Ι	0.469	0.045
Т	0.004	0.001
Р	-2.771	0.453

The coefficients and constant for multiple linear regression models of material removal rate (MRR) and surface roughness (Ra) are given in Equation 3 and Equation 4.

Multiple Linear Regression

MRR = -15.652 + 0.075R + 6.853I - 0.68T + (3)23.988P

$$Ra = 3.734 - 0.004R + 0.469I + 0.004T - 2.771P$$
(4)

## C. Optimization

Based on NSGA-II introduced by Deb et al. [1], a multiobjective optimization tool, MOGA using Matlab is applied to obtain the optimal solutions. MOGA acts on individuals with better fitness value that can help to increase the diversity of the population even if they have a lower fitness value. It is very important to preserve the diversity of population for convergence to an optimal Pareto front by controlling the elite members of the algorithm.

The steps start with initialization by generating the random population. The next step is evaluation of the fitness of each chromosome using the multi objectives function (machining models). The algorithm parameters boundaries (Table V) are used to get solutions that are within the expected values.

TABLE V. ALGORITHM BOUNDARIES

Parameters	Lower bound	Upper bound
Rotational speed, rpm	250	1000
Pulse current, A	5	15
Pulse on time, µs	200	1000
Flushing pressure,	0.5	1.5

Next is parent selection procedure which is based on the selection of fittest survival. The fittest chromosome from the current population is selected to generate new offspring. The selection is carried out using the binary tournament selection with crowded comparison operator. If the solutions belong to different fronts, one with a lower rank is selected. Meanwhile if the solutions belong to the same front, one with higher crowding distance is selected. Then crossover; new offspring is produce by combining subparts of selected chromosomes using recombination operator. Intermediate crossover is employed which creates two children from two parents. Mutation is carried out to introduce the deviation into chromosome to avoid premature convergence or segmentation. To improve the performance of genetic algorithm, elitist strategy is use to increase the speed of population domination. Using this strategy the best chromosomes are copied into the successive generation. Finally, termination of GA is when the stopping condition is satisfied; otherwise the circle will go to selection, crossover, mutation and so on for the next iteration. The flow repeats for successive generations. The final set of Pareto optimal solutions represents dominated solutions from the each generation and it is up to the decision maker to select a solution according to the selected objectives. The flow of MOGA optimization is illustrated in Figure 3.



#### Fig. 3. MOGA flow

The algorithm parameters for population, selection, mutation, crossover and generation are given in Table VI.

TABLE VI. ALGORITHM PARAMETERS

Parameters	Value	
Population size	100	
Selection - Tournament	4	
Mutation - Uniform	0.25	
Crossover - Intermediate	0.9	
Generation	1000	

## D. Results

MOGA is able to optimize more than one objective simultaneously resulted to time efficiency compared to single

objective genetic algorithm. Optimizing machining process parameters using SOP-MOGA and MLR-MOGA are expected to give best set of estimation solutions. The maximum removal rate (MRR), 152.660 mg/min and minimum surface roughness (Ra), 5.825  $\mu$ m values are obtained simultaneously using SOP-MOGA with *R*, *I*, *T*, *P* values are 978.929 rpm, 14.944 A, 212.372  $\mu$ s, 0.973 kg/cm<sup>2</sup> respectively. The same results of optimal solutions are generated twice as shown in Table VII. Figure 4 depicts the Pareto front of removal rate (MRR) and surface roughness (Ra) from SOP-MOGA optimization.

TABLE VII. SOP-MOGA OPTIMAL SOLUTIONS

	Sol.	Electrode	Current,	Pulse on	Flushing	MRR,	Ra,
		Rotation,	A (I)	time, µs	pressure,	mg/min	μm
		<b>rpm</b> ( <b>R</b> )		( <b>T</b> )	$kg/cm^2(P)$		
	1	979.175	5.799	211.907	0.975	93.620	8.790
	2	971.302	8.486	215.488	0.962	114.308	7.856
	3	978.929	14.944	212.372	0.973	152.660	5.825
	4	976.595	13.777	216.770	0.957	146.106	6.104
	5	976.378	11.294	215.180	0.963	133.030	7.051
	6	957.147	6.064	212.072	0.974	96.154	8.395
	7	976.557	11.752	216.432	0.958	135.406	6.858
	8	977.817	13.473	214.339	0.966	145.246	6.316
	9	976.987	14.075	216.031	0.960	147.728	6.019
	10	977.621	9.841	214.837	0.964	123.855	7.558
	11	977.232	7.179	213.438	0.969	104.700	8.367
	12	973.907	5.863	211.947	0.975	94.238	8.696
	13	977.763	12.217	214.566	0.965	138.525	6.769
	14	976.894	7.399	213.703	0.968	106.380	8.295
	15	978.170	14.589	213.601	0.968	150.753	5.913
	16	978.486	12.499	213.089	0.970	140.462	6.724
	17	978.702	11.047	212.788	0.972	132.096	7.240
	18	978.438	9.338	213.283	0.970	120.795	7.770
	19	977.347	11.528	214.157	0.967	134.672	7.016
	20	977.698	13.867	214.687	0.965	147.095	6.153
	21	978.282	13.153	212.501	0.973	144.106	6.500
	22	978.175	8.074	213.108	0.970	111.691	8.143
	23	978.816	8.096	212.583	0.972	111.975	8.160
	24	978.422	11.048	213.318	0.970	131.975	7.220
	25	978.601	9.378	212.764	0.972	121.193	7.774
	26	978.563	7.693	213.061	0.971	108.797	8.258
	27	977.472	7.206	213.260	0.970	104.959	8.368
	28	978.491	12.683	212.798	0.971	141.541	6.666
	29	979.062	6.606	212.066	0.974	100.368	8.581
	30	978.936	14.227	212.354	0.973	149.429	6.108
	31	978.952	13.675	212.324	0.973	146.784	6.321
	32	978.905	12.681	212.341	0.973	141.646	6.688
	33	974.213	6.130	211.988	0.975	96.500	8.633
	34	978.261	14.384	213.383	0.969	149.877	6.003
	35	977.593	8.271	212.379	0.973	113.349	8.097
	36	979.148	6.045	211.958	0.975	95.702	8.728
	37	977.590	12.029	213.885	0.968	137.647	6.853
	38	978.600	8.585	212.863	0.971	115.532	8.009
	39	978.381	12.482	213.301	0.970	140.314	6.722
	40	974.547	6.927	211.999	0.974	103.063	8.432
	41	978.023	11.476	213.413	0.969	134.542	7.066
	42	978.486	13.436	212.954	0.971	145.426	6.384
	43	976.054	5.837	211.931	0.975	93.987	8.734
	44	978.905	14.836	212.406	0.973	152.178	5.867
ļ	45	977.901	13.875	214.222	0.966	147.257	6.168
	46	978 686	10.676	212 399	0.973	129 881	7 374

Min	removal rate	(WIKK)			152.000	5 825
Mor	7/7.121	(MDD)	212.009	0.933	100.334	0.200
100	970.900	7 602	212.303	0.975	108 224	8 200
90	978.001	0.005	212.929	0.971	134 870	0.131
97	979.173	8 083	211.907	0.973	93.020 111.800	0.790
90	974.215	5 799	211.900	0.975	90.500	0.033 8 700
95	970.034	5.057	211.931	0.975	95.987	0./34
94	9/8.49/	11.504	213.11/	0.970	154./81	1.0/3
93	9/6.845	0.177	212.209	0.974	96.801 124 791	8.654
92	979.108	/.507	212.034	0.974	107.588	8.343
91	977.577	9.775	212.684	0.972	123.944	7.637
90	978.405	12.807	213.054	0.971	142.138	6.612
89	978.967	8.953	212.177	0.974	118.346	7.924
88	979.170	5.844	211.917	0.975	94.000	8.779
87	978.822	8.775	212.538	0.972	116.985	7.965
86	974.490	5.856	211.942	0.975	94.170	8.706
85	978.955	10.298	212.208	0.974	127.498	7.507
84	978.917	13.949	212.392	0.973	148.099	6.214
83	978.695	8.967	212.636	0.972	118.340	7.903
82	978.882	9.581	212.429	0.973	122.666	7.725
81	978.575	8.137	212.204	0.974	112.374	8.155
80	979.144	6.170	211.967	0.975	96.760	8.696
79	978.156	12.835	213.629	0.968	142.136	6.581
78	978.516	11.559	213.017	0.971	135.124	7.057
77	978.626	12.152	212.842	0.971	138.600	6.857
76	978.961	9.212	212.308	0.973	120.142	7.843
75	978.820	14.594	212.407	0.973	151.104	5.961
74	977.621	9.921	213.727	0.968	124.660	7.562
73	977.361	6.489	211.955	0.975	99.454	8.589
72	978.757	10.465	212.356	0.973	128.549	7.445
/1	9/8.46/	14.092	213.166	0.970	148.576	0.12/
70	9/8.081	10.150	212./34	0.972	120.409	1.000
09 70	9/8.044	0.398	212.401	0.975	114.277	8.00/ 7.525
60	970.014	9.370	212.332	0.972	122.303	1.124 8.067
0/ 69	9/8.905	13.519	212.410	0.975	143.982	0.3//
67	978.005	12 510	212.110	0.974	107.300	0.341 6 277
00 66	978.445	9.110	212.255	0.974	119.492	7.805 8.241
04 65	970.484 078 115	0.116	212.022	0.972	132.930	7 865
64	078 101	9.230	213.401	0.909	120.015	7 100
62	970.929	9 230	212.572	0.975	120.015	3.043 7 702
62	978.040	1/ 9//	214.055	0.907	123.339	7.514 5 875
61	978.046	10.069	212.929	0.971	125 550	7 514
60	978 551	8.083	212.407	0.975	114.995	8 151
50	978.017	12.942 9.409	212.303	0.973	145.055	0.366
58	979.072	12 9/2	212.000	0.974	1/3 035	0.J01 6 599
57	979.072	6 608	212.007	0.974	102.095	8 5 8 1
56	978.062	6.816	211.939	0.973	102.003	8 512
55	976 684	5.913	212.000	0.974	94 620	8 724
53	978.784	6 3 5 5	212.552	0.972	08 368	8 5 8 6
52	978 784	12 523	212.502	0.972	140 733	6.736
52	978.616	7 838	212.020	0.971	109.931	8 220
51	978.628	11 9/1	212.751	0.972	137.452	6.038
49 50	978.497	12 182	213.117	0.970	134.701	6.845
40	970.037	11 504	211.900	0.975	101.090	0.330
47	976.040	9.413	212.151	0.974	101.006	9.520
17	978 840	9.415	212 151	0.974	121 597	7 783



Fig. 4. Pareto front of MRR (objective 1) and Ra (objective 2) using SOP-MOGA

The optimal solutions of MLR-MOGA for removal rate and surface roughness are obtained separately as indicated in Table VIII. Maximum removal rate (MRR) is attained from the first set of solutions. While the optimal solutions for surface roughness is obtained from the second set of solutions. The maximum value for removal rate is 168.212 mg/min with combination of process parameters R = 974.770 rpm, I = 14.944 A, T = 218.250 µs and P = 0.967 kg/cm<sup>2</sup>. Meanwhile, the minimum surface roughness (Ra) is 0.693 µm and the process parameters are R = 977.810 rpm, I = 5.799 A, T = 211.907 µs and P = 0.973 kg/cm<sup>2</sup>. The Pareto front plots of removal rate (MRR) and surface roughness (Ra) using MLR-MOGA is shown in Figure 5.

TABLE VIII. MLR-MOGA OPTIMAL SOLUTIONS

	Electrode	Current,	Pulse on	Flushing	MRR,	Ra,
	Rotation,	A (I)	time, µs	pressure,	mg/min	μm
	$\operatorname{rpm}(R)$		(T)	kg/cm <sup>2</sup>		
				(P)		
1	974.770	14.944	218.250	0.967	168.212	5.038
2	977.810	5.799	211.907	0.973	106.366	0.693
3	977.546	6.595	212.461	0.931	110.743	1.187
4	977.620	6.382	212.341	0.949	109.726	1.037
5	976.302	10.391	215.067	0.946	136.852	2.940
6	977.718	6.059	212.102	0.953	107.639	0.872
7	975.848	12.221	216.048	0.953	149.464	3.785
8	976.860	9.275	213.910	0.951	129.437	2.398
9	976.924	8.583	213.764	0.946	124.585	2.086
10	975.560	12.651	216.603	0.960	152.523	3.970
11	977.503	6.734	212.549	0.964	112.471	1.162
12	974.938	14.946	217.900	0.964	168.206	5.043
13	976.172	10.984	215.342	0.958	141.177	3.187
14	976.300	10.556	215.072	0.960	138.325	2.978

15	975.560	13.215	216.603	0.960	156.389	4.235
10	077.000	7.625	210.002	0.061	110.500	1.505
10	977.230	7.635	213.123	0.961	118.528	1.595
17	976.805	8.834	214.007	0.961	126.634	2.164
10	075 426	12 020	216 996	0.066	156 605	4 220
10	975.420	13.232	210.000	0.900	150.005	4.230
19	975.928	11.525	215.878	0.962	144.919	3.433
20	077 322	7 252	212 027	0.956	115 787	1 / 30
20	711.322	1.252	212.927	0.750	115.767	1.450
21	976.711	9.113	214.205	0.964	128.619	2.286
22	977 810	5 799	211 907	0.966	106 190	0713
22	075.027	11 000	211.907	0.900	147.225	2 (12
23	975.837	11.888	216.055	0.959	147.325	3.612
24	976.222	10.642	215.247	0.963	138.948	3.013
25	076 488	0.873	214 708	0.061	133 685	2 656
25	970.400	9.873	214.708	0.901	155.065	2.050
26	976.320	10.358	215.028	0.950	136.716	2.915
27	976 683	9 240	214 270	0.956	129 274	2 370
20	076.005	10.1.0	214.270	0.950	125.274	2.570
28	970.395	10.169	214.902	0.960	135.072	2.798
29	975.050	14.124	217.676	0.965	162.607	4.655
30	076 506	0 5/18	214 449	0.961	131 / 85	2 502
50	770.370	J.J+0	214.44)	0.901	151.405	2.302
31	975.785	12.409	216.152	0.960	150.901	3.855
32	974.878	14.629	218.026	0.966	166.075	4.890
22	075 027	11 000	216.055	0.050	147.225	2 (12
33	975.857	11.888	216.055	0.959	147.525	3.012
34	976.544	9.664	214.561	0.963	132.320	2.551
35	975 866	11 706	215 967	0.956	146 009	3 536
55	775.000	11.700	213.907	0.750	140.007	3.330
36	975.910	11.515	215.872	0.969	145.022	3.409
37	977.546	6.598	212.458	0.973	111.767	1.073
20	074 702	14.970	218 202	0.07	1(7 771	5.007
38	974.795	14.879	218.203	0.967	10/.//1	5.007
39	975.366	13.457	217.020	0.963	158.060	4.344
40	977 220	7 617	213 140	0.970	118 615	1 562
40	777.220	7.017	213.140	0.970	110.013	1.302
41	976.283	10.402	215.098	0.965	137.369	2.894
42	976.599	9.531	214.474	0.961	131.386	2.492
12	077 262	7 160	212.945	0.060	115 500	1 240
43	977.303	1.162	212.845	0.969	115.509	1.349
44	977.810	5.799	211.907	0.973	106.366	0.693
45	976 960	8 360	213 684	0.969	123 621	1 917
40	075.100	14,000	215.004	0.909	162.667	1.717
46	975.129	14.280	217.506	0.964	163.667	4./30
47	975.272	13.436	217.207	0.965	157.942	4.330
10	076 510	0.799	214 622	0.062	122 155	2 610
40	970.510	9.700	214.052	0.902	155.155	2.010
49	977.058	8.088	213.481	0.969	121.787	1.787
50	977 470	6 846	212 621	0 969	113 356	1 201
50	076 100	10.000	212.021	0.909	110.000	1.201
51	976.180	10.888	215.317	0.965	140.689	3.122
52	976.188	11.018	215.305	0.964	141.551	3.187
53	077 308	7 357	212 088	0.051	116 400	1 402
55	977.308	1.557	212.900	0.951	110.400	1.492
54	975.164	13.758	217.428	0.967	160.185	4.476
55	976 348	10 566	214 973	0.963	138 469	2 975
55	076.025	10.300	214.973	0.705	126.520	2.975
56	976.335	10.280	214.993	0.964	130.539	2.838
57	975.462	13.059	216.814	0.962	155.322	4.159
58	976 118	10 891	215 439	0.970	140 798	3 1 1 3
50	970.110	10.071	213.437	0.970	140.790	5.115
59	977.170	7.734	213.244	0.966	119.320	1.627
60	975.866	11.706	215.967	0.956	146.009	3.536
61	074 878	14 620	218 026	0.066	166.075	1 800
01	974.070	14.029	218.020	0.900	100.075	4.890
62	977.620	6.382	212.341	0.949	109.726	1.037
63	976 962	8 353	213 677	0.971	123 633	1 907
65	075.160	12 992	215.077	0.071	160.045	1.507
64	975.168	13.883	217.433	0.963	160.945	4.545
65	976.842	8.714	213.929	0.971	126.070	2.079
66	075 564	12 052	216 610	0.062	154 611	4 108
00	775.504	12.752	210.010	0.702	134.011	4.100
67	977.570	6.536	212.411	0.972	111.329	1.046
68	975.966	11.469	215.761	0.963	144,571	3.404
60	077 021	9 160	212 527	0.040	122.200	1 0 10
09	977.031	8.169	213.337	0.968	122.309	1.828
70	975.527	12.692	216.676	0.967	152.954	3.972
71	975 170	14 081	217 401	0.964	167 373	4 635
11	) 1 3.1 1 7	14.001	217.401	0.704	102.323	1.000
72	977.345	7.272	212.880	0.972	116.316	1.394
73	975.855	11.680	215.986	0.969	146.139	3.487
71	075 742	12 024	216 222	0.060	149 520	3 650
/4	713.143	12.030	210.223	0.908	146.550	5.058
75	976.235	10.767	215.207	0.966	139.878	3.064
76	975 977	11 329	215 739	0.968	143 727	3,325
	075 040	11.242	215.757	0.200	142.050	2.225
11	973.968	11.342	215.752	0.969	143.850	5.526
78	975.942	11.468	215.825	0.964	144.591	3,399

83 84 85 86 87 88 89 90 91 92 93 94 92 93 94 95 96 97 98 99 98 99 99 90 97 98 99 90 97 98 99 90 90 97 98 99 90 90 90 90 90 90 90 90 90 90 90 90	976.947 977.287 976.603 975.234 975.234 975.126 976.126 975.146 977.810 977.810 974.770	8.452 7.396 9.503 13.548 11.916 11.127 13.944 5.799 14.944	213.710 213.003 214.430 217.282 216.144 215.425 217.479 211.907 218.250	0.969 0.965 0.967 0.967 0.968 0.967 0.963 0.966 0.967	124.251 116.995 131.319 158.765 147.712 142.362 161.363 106.190 168.212	4.209 1.960 1.471 2.464 4.376 3.602 3.229 4.574 0.713 5.038
83       84       9         84       85       9         85       86       9         87       88       9         90       9       9         91       9       9         92       9       9         93       9       9         94       9       9         95       9       9         96       9       9         98       9       9         90       9       9         90       9       9         90       9       9         90       9       9         90       9       9         90       9       9         90       9       9         90       9       9         90       9       9         90       9       9         90       9       9         99       9       9         100       9       9	976.947 977.287 976.603 975.234 975.780 976.126 975.146 977.810 974.770	8.452 7.396 9.503 13.548 11.916 11.127 13.944 5.799 14.944	213.710 213.003 214.430 217.282 216.144 215.425 217.479 211.907 218.250	0.969 0.965 0.967 0.967 0.968 0.967 0.963 0.966 0.967	124.251 116.995 131.319 158.765 147.712 142.362 161.363 106.190 168.212	4.209 1.960 1.471 2.464 4.376 3.602 3.229 4.574 0.713 5.038
83       84       9         84       85       9         85       86       9         87       9       9         90       9       9         91       9       9         92       9       9         93       9       9         94       9       9         95       9       9         96       9       9         98       9       9	976.947 977.287 976.603 975.234 975.780 976.126 975.146 977.810	8.452 7.396 9.503 13.548 11.916 11.127 13.944 5.799	213.710 213.003 214.430 217.282 216.144 215.425 217.479 211.907	0.969 0.965 0.967 0.967 0.968 0.967 0.968 0.967 0.963 0.966	124.251 116.995 131.319 158.765 147.712 142.362 161.363 106.190	4.209 1.960 1.471 2.464 4.376 3.602 3.229 4.574 0.713
83       84       9         84       85       9         85       86       9         87       9       9         90       9       9         91       9       9         92       9       9         93       9       9         94       9       9         95       9       9         97       9       9         98       9       9	976.947 977.287 976.603 975.234 975.780 976.126 975.146	8.452 7.396 9.503 13.548 11.916 11.127 13.944	213.710 213.003 214.430 217.282 216.144 215.425 217.479	0.969 0.965 0.967 0.967 0.968 0.967 0.963	124.251 116.995 131.319 158.765 147.712 142.362 161.363	4.209 1.960 1.471 2.464 4.376 3.602 3.229 4.574
83       84       9         84       85       9         85       86       9         87       9       9         90       9       9         91       9       9         92       9       9         93       9       9         94       9       9         95       9       9         96       9       9	976.947 977.287 976.603 975.234 975.780 976.126	8.452 7.396 9.503 13.548 11.916 11.127	213.710 213.003 214.430 217.282 216.144 215.425	0.969 0.965 0.967 0.967 0.968 0.967	124.251 116.995 131.319 158.765 147.712 142.362	1.209 1.960 1.471 2.464 4.376 3.602 3.229
83 84 85 86 87 88 89 90 91 92 93 92 93 94 95 96	976.947 977.287 976.603 975.234 975.780	8.452 7.396 9.503 13.548 11.916	213.710 213.003 214.430 217.282 216.144	0.969 0.965 0.967 0.967 0.968	124.251 116.995 131.319 158.765 147.712	4.209 1.960 1.471 2.464 4.376 3.602
83 84 85 86 87 88 89 90 91 92 93 94 95	976.947 977.287 976.603 975.234	8.452 7.396 9.503 13.548	213.710 213.003 214.430 217.282	0.969 0.965 0.967 0.967	124.251 116.995 131.319 158.765	4.209 1.960 1.471 2.464 4.376
83 84 85 86 87 88 89 90 91 92 93 94	976.947 977.287 976.603	8.452 7.396 9.503	213.710 213.003 214.430	0.969 0.965 0.967	124.251 116.995 131.319	4.209 1.960 1.471 2.464
83 84 85 86 87 88 89 90 91 92 93	976.947 977.287	8.452 7.396	213.710 213.003	0.969 0.965	124.251 116.995	4.209 1.960 1.471
83 84 85 86 87 88 89 90 91 92	976.947	8.452	213.710	0.969	124.251	4.209
83 84 85 86 87 88 89 90 91				0.201	150.520	4.209
83 84 85 86 87 88 89 90	975.358	13.191	217.027	0.967	156 328	4 200
83 84 85 86 87 88 88 89 89	977.728	6.053	212.080	0.966	107.920	0.832
83 84 85 86 87 88 88	976.725	9.167	214.174	0.969	129.101	2.298
83 84 85 86 87 87	975.615	12.404	216.488	0.968	151.037	3.831
83 9 84 9 85 9 86 9	976.133	11.221	215.421	0.963	142.910	3.285
83 9 84 9 85 9	976.507	9.773	214.633	0.965	133.118	2.595
83 9 84 9	975.010	14.410	217.752	0.965	164.576	4.789
83 9	977.266	7.478	213.043	0.972	117.710	1.492
	976.329	10.283	214.999	0.969	136.671	2.825
82 9	977.017	8.187	213.564	0.972	122.513	1.828
81 9	7/0.314	9.915	214.619	0.966	134.121	2.659
80 9	076 514	6.111	212.122	0.971	108.429	0.847
79	977.708		212.294	0.971	110.168	0.968



Fig. 5. Pareto front of MRR (objective 1) and Ra (objective 2) using MLR-MOGA

Table IX shows the maximum removal rate and minimum surface roughness obtained from SOP-MOGA and MLR-MOGA. T test were conducted to validate the differences between experimental with SOP-MOGA and MLR- MOGA optimization. If p < 0.05, it shows that the observed different within two methods are significant. Value of p for SOP-MOGA and MLR-MOGA are given in Table X, whereby p values of removal rate are 4.599E-05 and 8.016E-07 respectively. Therefore, both optimization techniques are statistically significant, however MLR-MOGA shows better confidence interval. The t test for validation of surface

roughness value is shown in Table XI. The p values of SOP-MOGA and MLR-MOGA are 0.000517533 and 8.138E-05 respectively. The differences in surface roughness between experimental with SOP-MOGA and MLR-MOGA are also considered to be statistically significant. Though, p value of surface roughness is lower when using MLR-MOGA and provides better confidence level than SOP-MOGA.

TABLE IX. MLR-MOGA OPTIMAL SOLUTIONS

Model- Optimization	Electrode Rotation, rpm (R)	Current, A (I)	Pulse on time, μs (T)	Flushing pressure, kg/cm <sup>2</sup> (P)	<i>MRR</i> , mg/min	<i>Ra</i> , µm
SOP-MOGA	978.929	14.944	212.372	0.973	152.660	5.825
MLR-MOGA	974.770 977.810	14.944 5.799	218.250 211.907	0.967 0.973	<b>168.212</b> 106.366	5.038 <b>0.693</b>

TABLE X. RESULT COMPARISON OF MRR

MRR	Experimental	SOP-MOGA	MLR-MOGA
Mean	82.235185	123.26438	136.57759
Variance	2090.1961	350.06605	328.6352
Observations	27	100	100
Hypothesized Mean Difference		0	0
df		28	28
t Stat		-4.561184	-6.0492194
P(T<=t) one-tail		4.599E-05	8.016E-07
t Critical one-tail		1.7011309	1.7011309
P(T<=t) two-tail		9.197E-05	1.603E-06
t Critical two-tail		2.0484071	2.0484071

TABLE XI. RESULT COMPARISON OF RA

Ra	Experimental	SOP-MOGA	MLR-MOGA
Mean	5.378148148	7.5066018	2.8434038
Variance	8.826023362	0.8302611	1.5969289
Observations	27	100	100
Hypothesized Mean Difference		0	0
df		27	29
t Stat		-3.676352422	4.3288881
P(T<=t) one-tail		0.000517533	8.138E-05
t Critical one-tail		1.703288423	1.699127
P(T<=t) two-tail		0.001035066	0.0001628
t Critical two-tail		2.051830493	2.0452296

## **III. CONCLUSION**

This paper presented comparative empirical results of using two types of regression models to integrate with multiobjective GA. Most researchers used second order polynomial regression [18, 20, 21, 22]. Lower level of regression model, multiple linear regression is used in this study to compare the efficiency of these two techniques when integrating it with multi objective optimization, as in this case, MOGA is used. Generally, SOP-MOGA and MLR-MOGA are relevant in optimizing machining process parameters. The results proved that the best removal rate (MRR) and surface roughness (Ra) are obtained from MLR-MOGA. However, SOP-MOGA is able to generate possible maximum removal rate (MRR) and minimum surface roughness (Ra) values simultaneously from same solution without neglecting any of the objectives. From the results of MLR-MOGA, operators and engineers can choose either to maximize removal rate (MRR) or minimize surface roughness (Ra).

## ACKNOWLEDGMENT

The authors highly appreciate the editors and reviewers for useful advices and positive comments. This work is partially sponsored by the Research Management Centre (RMC), Universiti Teknologi Malaysia (UTM) and Ministry of Higher Education Malaysia (MOHE) for funding throughout the Fundamental Research Grant Scheme (FRGS) vot. No. R.J130000.7828.4F721

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